LECTURE NOTES

ON

FLUID MECHANICS

4th SEMESTER MECHANICAL

BY

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MODEL SET QUESTION FOR PRACTICE

SUB: - FM (Fluid Mechanis) SET-1 Time-3 hours. Full Marily -80 Answer any fine questions including question NIO-01, and 02. (1 (a) Define Specific weight and specific granity. 12×10 (b) Define pressure and state its unit. (c) Define the terror viscocity Write Anchimedis's preinciple. (e) Define metacentre and metacentric height. (f) what is the difference between laminar and turbulent flow? (g) what is pitot tube ? (h) state Darcuy's formely for loss of head in pipe ? (is what do you mean by impart of jet ." (j) what is venucontracta? 5X6 (2) Answer any five. (i) with near sketch enplain the working of Bourden's tube pressure gauge. (ii) Derieve an equation for the total pressure on a verdical immergeef surface. (iii) The diameter of a pipe at the section 1 and 2 are 10 cm and 15 cm respectively. Find the discharge through the pipe if the velocity of coater flowing through the pipe at rection G is sm/s. Find the velocity at section 2. (iv) write down the expression of loss of every due to friction according to Davay's formula and cheruja formula with proper notation. $\begin{bmatrix} I \end{bmatrix}$

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- (V) A sharp-edgesed onifice of scm diameter dischanges water under a head of 45m. Determine the coefficient of discharge is the measured rate of flow is 0.0122m³/. (vi) Derive an expression for the force of jet on a fired plate.
- (3) A rectangular plane surface is 2m wide and 3m¹³ deep. It lies in writical plane in water. Determine the fotal pressure and position of centre of processes on the plane surface when its opper edge is hereitental and councides with the water surfaces. also find the total pressure and position of centre of processes when the opper edge is 2.5m below the free couler surface. (Y) Describe the orifice coefficiences and write elson 10 the relationship among them.

(5) Waler flows through a pipe of 200mm in eligencler and Gom long with a velocity of 2.5m/s. Find the head lost due to fraition using

(a)Darcuj, formula, f= 0.005

(b) chozuj's formula C = 55.

(6) Derive Bernoulli's equation and state the prioritical application in venturimeter.

(7) A jet of water 40 mm cliamler moving with a velocity of 120m/s impinging on a reries of varies [10] moving with a velocity of 5m/sec. Find the force evented, workdone and efficiency.

All The Best.

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MODEL SET QUESTION FOR PRACTICE sul: - Fluid Mechanics . SET-2] Time - 3 hours Full Mennes- 20 Answer any fine questions including question No. 01 and 02. Duppefine density and state its unit. 12×10 (ii) Define pascel's law. (iii) Define the team surface tension. (IV) what is the function of pierometers? (v) Define Bovyany force .) (Vi) what is the difference between compressible and incompressible fluid (vii) what are the assumptions taken in deriving the Bernoulli's equation. (viii) what is chezy's constant? (1x) Define hydraulic greaclient? (n) Define pressure head and nelocity head. 3(1) Explain abable pressure, almospheric pressure and gauge pressure and state their relations. (ii) Explain the working and function of a pitot tube. (tii) A simple U-tube manometor containing mercury is connected to a pipe in which fluid of specific graning 0.8 end having vaccum pressure is flowing. The other end of the manometer is open to atmosphere. Find the volum pressure in the pipe if the difference of menery level in the two limbs is your and the height of fluid in the left from the centre of pipe in 15cm. below. (iv) Dereine continuity equation.

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(V) water is flowing through a pipe 1500 m long and 400 mon diameter with a velocity of 0.7 m/s. what should be the diameters of pipe if the loss of head due to fruction is 8.7 m. Take of -for the pipe is 0.01. (vi) Enplain hydraulic gradient and total gradient 10 line . (3) Describe clifferent types of manometers. (y) The head of water over an oriefice of climeter yomm in 10m. Find the actual discharge and actual velocity of jet at vena contracta. take (d = 0.6, Cv = 0.98. (i) The discharge over a rectangular notch is 0.135 m³/s when the water level is 22.5 m above the still. if the coefficient of clincharage in 0.6 find the 15 (5) Dervine an enprovion for the force of jet on a [10 fined and inclined plate. length of notch. <6> Desuribe different types of flows ' [10 (7) Derive the expression of actual discharge in [10 venturimeter and state its practical applications.

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 $\left[2\right]$

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NOTCHES AND WEIRS

and Dr. asta (1 g.) Introduction 7 A notch is a clevice used for measuring the reife of flow of a liquid through a small channel or a tank ->91 may be defined as an opening in the ricle of a tank on a small channel in such a way that the fiquid surfaces in the tank or channel is below the top edge of the opening -> A weire às a concrete strature ; planet in as open channel over which the flow occurs. 9+ in generally in the form of vertical wall with a sharp edge cet the top. -> The notch is of small size while the weir is of a bigger iere > The notch is generally made of metallic plate while the wein is made of concrete streeture. clamitication The notches are clamified as OAccording to the chape of motes opening (i) reetangular notch (11) Trianguleur notch (iii) Traporoidal notch (iv)stepped notch. @According to the effect, of the rider of naple: -(i) Notch with end contraction (ii) Notch without end contraction. weires are classifief awreling to chape (9) According to the shape of opening (1) Reutanguler wein (ii) Triangulaire Weire (iii) Traperoidal weire.

(b) According to the chape of crest (i) sharep-crested weire (ii) Narrow - crested wein (iii) Bound-cresteef wein house (iv) og ee - shapael weire in human (c) Accorcling to the effect of ricles on the Emerging nappe! -(i) wein with end contraction with (ii) wein without end contraction. DISCHARGE OVER A RECTANGULAR NOTCH 1 P 1- WFIL edge al the top. INAIPE. Du Dogn to 1.5 Asl. Ь] generally mode 11 11 time the 1000 Le weire 1.3 (AD) KANDON cloui ice au Reetanguleer Notch IL of primary (1) rectaged estappints til tracco Traps calelas the water of rappo crest 110/2011 reting to the offer (i)Molth with and all markens Rectanguleite Weire Jugit du du i heims and claquinge-1 garancelle 19) According to Mr. Atops of ppeaking 1) Reuter Julian wine Such 13 1175 ' Fun as F 1 1

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consider a rectangular notch on wein provided
in a channel carraying water.
H = head of avalen over the crest
L = Length 0.1 The notch on wein.
To find the discharge of water flowing over
the wein on notch, consider an elementary
honizontal strip 0.1 water 0.1 thickness dh and
length L at a depth h from the free surface.
Areas 0.1 Strip = L×dh.
theoretical velowity 0.1 water theowing through
strip =
$$\sqrt{2gh}$$

The discharge do, through strip c_1
 $dg = Cd \times areas of strip × Theoretical velowity$
 $dg = Cd \times areas of strip × Theoretical velowity$
 $dg = Cd \times L \times \sqrt{2gh} \times dh$
 $= cd \times L \times \sqrt{2gh} \times dh$
 $= cd \times L \times \sqrt{2g} \times \frac{h^{3/2}}{3/2} \int_{0}^{H}$
 $= Cd \times L \times \sqrt{2g} \times \frac{h^{3/2}}{3/2} \int_{0}^{H}$
 $= Cd \times L \times \sqrt{2g} \times \frac{h^{3/2}}{3/2} \int_{0}^{H}$
 $= Cd \times L \times \sqrt{2g} \times \frac{h^{3/2}}{3/2} \int_{0}^{H}$
 $= Cd \times L \times \sqrt{2g} \times \frac{h^{3/2}}{3/2} \int_{0}^{H}$
 $= Cd \times L \times \sqrt{2g} \times \frac{h^{3/2}}{3/2} \int_{0}^{H}$
 $= Cd \times L \times \sqrt{2g} \times \frac{h^{3/2}}{3/2} \int_{0}^{H}$
 $= Cd \times L \times \sqrt{2g} \times \frac{h^{3/2}}{3/2} \int_{0}^{H}$
 $= Cd \times L \times \sqrt{2g} \times \frac{h^{3/2}}{3} \times (H)^{3/2}$

ST

9) Find the diversary of walen flowing owen
rectangular notes of 2m length when the units
here over the notifier of 300 mm to 500
Here over the notifier of 300 mm to 300

$$C_{d} = 0.60^{11}$$
 $L = 2m$
 $C_{d} = 0.60^{11}$ $L = 2m$
 $C_{d} = 0.552^{m}/S$
 $C_{d} = 0.61^{11}$
 $C_{d} = 0.62^{11}$
 $C_{d} = 0.323^{m}/S$
 $C_{d} = 0.323^{m}/S$
 $C_{d} = 0.323^{m}/S$
 $C_{d} = 0.323^{m}/S$

OVER A TRIANGULAR NOTCH OR WEIR

DISCHARGE

H=head of water above the V-notch. a=angle of notch. consider the horizontal strip of coater of thickness 'dh' at a clepth of h from the free uniferer of water. $\tan \theta_2 = \frac{Ac}{oc} = \frac{Ac}{(H-h)}$ $Ac = (ht - h) tan \frac{0}{2}$ AB = width of strip = 2x AC = 2x (H-h) tan 0/2 x db (ach' 2 and) theoratical velocity of water through streep = 1296 Discharcye through the strip de = Cy x Area of strip x velocity = Cq X 2(H-h) ton % Xdh X 295 = 2× (4×(+-h) tan 1/2 × v2gh × dh a = "J 2 cy × (H-h) tan @/2 × J2gh × dh = 2 cq x tan $\frac{1}{2} \times \sqrt{29} \times \int (1+h) h^{1/2} dh$ = 2x Cd x tan 0/2 x V 29 [] H h 1/2 dh - Jh 3/2 dh] = 2x cd x tom a/ x V2g [2/3 H - 2/5 H 5/2] = 2X (q X tan 0/2 X / 29 X (1/15 H) (53)

Q = % 15 Cyx tan 0/2 X J29 X H 5/2 for a V-notch Cy=0. C $Q = q \delta^{\circ}, t c n \delta^{\prime}_{2} = 1.$ $Q = \frac{8}{15} \times 0.6 \times 1 \times \sqrt{29} \times H$ $Q = 1.417H^{5/2}$ 1) Find the discharge over a trieunguleur notch of angle Go° when the hered over the V-notch in 0.3m Astar No Co = 0.6 AMANINO = Goord Los quille los mois of #= 0:3 m. sil all mail- d la diplo Cy = 0.6 Q = 8/15 × Cq × tan 0/2 × 29 × H5/2 = $\frac{8}{15} \times 0.6 \times \tan 30^{\circ} \times \sqrt{2 \times 9.81} \times (0.3)^{5/2}$ $Q = 0.040 m^3/s. (Ans) d/ox 20 mod (4-4) x.$ respected reported of andre philosoft straip = 1036 ande Through The Midp 2 = Cop Arcon Col adric por the "mining 365 x 46x 20 mot (4-4) 5 x 60 -At x G x C H-H) - L-M CAXX - 345 x H 1 = Cal X (H- H) 1 = a Cal X - 2 - 3 - 4 - X - 14 44 44 (1-41) × 1 + 10 mot x 621 = all - at stand from to mot x to as N' R & Mar North Start S

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FLOW THROUGH PIPES (CHAPTER-G) Alexand. Lou of energy in pipe. an when a fluid in flowing through a pipe, the fluid experiences some reinstance due to which some of the energy of fluid is lost. This low of overagy in clauifiel as follous. Eenergy loss boundary stid to them -In Calo Che Major energy loss no diges min Minor energy loss (a) Sudden enpanion of pipe Then in due to freiction. (b), Suelclen contraction of pipe (a 1 Darcey - Weis beech formules ... (c) Bend in pipe ! (b) cherry's Formula. (d) pipe tittings me, - Obstruction in pipe. UN LOAR of energy due to traction. (a) Durry-Weisbach Formula: This loss of energy in pipes due to frietion is calculated from Dancy-Weisbach equation. $\int h_f = \frac{4fLV^2}{2gq}$ hy = Loss of head due to freition. f = Coefficient of friction = 16 Ro 2112013 $f = \frac{16}{R_0} \left(R_e < 2000 \right)$ $f = \frac{0.079}{10^{1/9}} \left(Re \left(4000 - 10^{6} \right) \right).$ $j \times m / X = V$. L=Length of pipe. V = mean velocity of flow of = diameters of pipe. W = M B

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(b) cherry's formula
The expression for low at heaved due to thick.

$$h_{f} = \frac{f^{2}}{f^{3}} \times \frac{h}{h} \times L \times V^{2}$$

$$h_{f} = low of heaved due to friction
$$h_{f} = source of heaved due to friction
$$h_{f} = source of the count - received of pipe
A = water perimeter of pipe.
$$\frac{h}{p} = perimeter of pipe.
$$\frac{h}{p} = perimeter of pipe.
$$\frac{h}{p} = perimeter depth or hydroculic means due
$$\frac{h}{p} = (hydroculic mean depth or hydroculic means due
$$\frac{h}{p} = m \text{ or } (\frac{f}{p}) = l/m.$$

$$h_{f} = \frac{f'}{3} \times L \times V^{2} \times \frac{h}{m}.$$

$$h_{f} = \frac{f'}{f} \times L \times V^{2} \times \frac{h}{m}.$$

$$h_{f} = \frac{f'}{f} \times m \times (\frac{1}{L})$$

$$V = (\frac{59}{f^{1}} \times m \times (\frac{1}{L}))$$

$$h_{f} = i$$

$$(V = C \times \sqrt{m \times i}]$$
This is known as cherry's formulae.$$$$$$$$$$$$$$

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a), Find the diameter of pipe of length 2000 when the rate of flow of water through the pipe in 200 diterry/see and head loss dee to fraction is ym -C = 501 6 1 1 1 Aug L = 2000 m. Q = 2000litre/s = 0.2 m3/s. hr = ym. $C = 50 - V = \frac{direhangel \times 1 - 0.2^{E \cdot C \times E}}{Ancer} (\frac{1}{T_{y}} d^{2l})^{100}}$ $V = C \times \sqrt{mc} (\frac{1}{T_{y}} d^{2l})^{100}$ $V = 50 \times \sqrt{\frac{1}{9} \times \frac{h_{1}}{L_{1}}} + \frac{V \times 1 \times 1}{V \times 1 \times 1}$ $\frac{0.2 \times 1}{T_{y}} = 50 \times \sqrt{\frac{1}{9} \times \frac{y}{2000}}$ $\frac{V \times 1}{T_{y}} d^{2}$ C = 50. $\frac{T}{Y_{4}} = \frac{0.2 \times 10^{-1}}{T_{4} d^{2} \times 50} = \sqrt{\frac{d}{4}} \times \frac{\frac{14}{7} \cdot 1}{2000} = \sqrt{\frac{3}{7}} \times \frac{14}{2000} = \sqrt{\frac{3}{7}} \times \frac{14}{200} = \sqrt{\frac{3}{7}} \times$ $\Rightarrow \left(\frac{0.2 \times 4}{\pi d^2 x s^{\infty}}\right)^2 = \frac{d}{2000}$ $\Rightarrow \frac{(0 \cdot 2)^{2} \times (4)^{2}}{\pi^{2} \times 4^{4} \times (50)^{2}} = \frac{4}{2000}$ $\Rightarrow \frac{(0 \cdot 2)^{2} \times 16 \times 2000}{\pi^{2} \times (50)^{2}} = 4^{5}$ =7 q = $\sqrt{0.0518}$ = 0.553m = 53mm (And)

Minore Energy Losses :- The loss of energy due to friection in pipe is Known ers major loss while the loss of every cleve to change of nelociety of the for fluid in called minor loss of energy OLOSA Of head due to udden enlangement->₩2 V1 Protone with me free is with me at consider a liquid flowing through a pipe which has sudden enlargement as shown on rebone figure. consider two rections O-O and O-O before and after enlangementer, 1= chat-(11-ch) 1+1419 - 1 P, = pressure intenity at section 0-0 VI = velocity of flow at section @-0 a, = area of pipe at rection O-O. P2 = presume intervity set section 2 - 2. V2 = velocity of flow at rection @-@ az = anea of pipe at section @-@ > Due to sudden change in diameter of pipe from D1 to D2, the liquid flowing from the smaller,

DI to Dz, the liquid flowing from the smaller, pipe is not able to follow the change of boundary. Thus the flow separates from the boundary and turbulent eddies are formed.

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The loss of energy topses place due to topse
of those coldies:

$$p^{2} = pressure intensity of the liquic dialogs
he = Loss of head also to subdem enhancement
he = Loss of head also to subdem enhancement
he = Loss of head also to subdem enhancement
he = Loss of head also to subdem enhancement
 $\frac{P_{1}}{4g} + \frac{v_{1}^{2}}{2g} + z_{1} = \frac{P_{2}}{3g} + \frac{v_{2}^{2}}{2g} + Z_{2} + head loss
= \frac{P_{1}}{4g} + \frac{v_{1}^{2}}{2g} = \frac{P_{2}}{3g} + \frac{v_{2}^{2}}{2g} + Z_{2} + head loss
= \frac{P_{1}}{5g} + \frac{v_{1}^{2}}{2g} = \frac{P_{2}}{3g} + \frac{v_{2}^{2}}{2g} + he
= \frac{P_{1}}{5g} + \frac{v_{1}^{2}}{2g} = \frac{P_{2}}{3g} + \frac{v_{2}^{2}}{2g} + he
= he = \left(\frac{P_{1}}{5g} - \frac{P_{1}}{3g}\right) + \left(\frac{v_{1}^{2}}{2g} - \frac{v_{2}^{2}}{2g}\right)$
= The force acting on the liquid in the control
volume in the discretion of flags is given by
 $\left[\frac{F_{1}}{F_{2}} = P_{1}A_{1} + P_{1}(A_{2} - A_{1}) - P_{2}A_{2} - P_{1}A_{2} - P_{2}A_{2}\right]$
For $P_{1}A_{1} + P_{1}(A_{2} - A_{1}) - P_{2}A_{2} = P_{1}A_{2} - P_{2}A_{2}$
 $\left[\frac{F_{1}}{F_{2}} = A_{2}(R - P_{2})\right]$
Momentum of liquid at section $1 - 1 = g_{1}A_{1}v_{2}^{2}$
 $change in momentum $g_{1}A_{2}v_{2}^{2} - g_{1}A_{2}v_{2}^{2}$
 $change in momentum $g_{2}A_{2}v_{2}^{2} - g_{1}A_{1}v_{2}^{2}$
 $\left[\frac{A_{1}}{A_{1}} = \frac{A_{2}v_{2}}{v_{1}}\right]$
 $change in momentum $f_{1}e_{1} = g_{2}A_{2}v_{2}^{2} - g_{1}A_{2}v_{2}^{2}$
 $f_{1}A_{2}v_{2}^{2} - g_{2}x_{1}A_{2}v_{2}^{2} + g_{2}A_{2}v_{2}^{2}$
 $f_{2}A_{2}v_{2}^{2} - g_{2}x_{1}A_{2}v_{2}^{2} + g_{2}A_{2}v_{1}v_{2}^{2}$
 $= f_{2}A_{2}v_{2}^{2} - g_{2}x_{1}A_{2}v_{2}^{2}$$$$$$

Net force acting on control volume in the direction of flow must be equal to the reate of change of momentum $(P_1 - P_2) = SA_2 (V_2^2 - V_1 V_2) \qquad \text{org} \qquad \text{org}$ $= V_2 - V_1 V_2$ with the reasonable to reasonable the materials Masarth minim $= \frac{1}{2} \left[\frac{P_1 - P_2}{S_1 + 1} - \frac{V_2^2 - V_1 V_2}{S_1 + 1} \right] = \frac{V_2 - V_1 V_2}{S_1 + 1} \left[\frac{V_2 - V_1 V_2}{S_1 + 1} \right] = \frac{V_2 - V_1 V_2}{S_1 + 1} \right]$ $he = \left(\frac{P_{12}}{89} - \frac{P_{2}}{89}\right) + \left(\frac{V_{12}}{29} - \frac{V_{2}^{2}}{29}\right) \dots$ [used Lo was int] $= \frac{v_2^2 - v_1v_2}{2g} = \pm \frac{v_3^2}{2g} = \frac{v_2^2}{2g}$ 222 - 22122 + 292 - 222 -S-S proition 2. 1 - 1 Lou prision 2-2. N2 + V12 - 2V1 V2- found to mad and continution S(1- 24 - 21)2 $he = \frac{(v_1 - v_2)^2}{2q}$ of Head dere to Sudders Contraction From continuity equation [nove - A.V. Low - KP2A2 PIN \mathcal{O} CP

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$$\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \end{array}{} \end{tion} \end{ti$$

where $K = \left(\frac{1}{C_c} - 1\right)^2$ $h_{c} = \frac{kv_{2}^{2}}{2gr}$ when a disput f entern or p et april of factures $C_{c} = 0.62$ $K = \left(\frac{1}{0.62} - 1\right)^2 = 0.375^{-1}$ $hc = 0.375 \frac{V2^2}{2.9}$ + -If the covalue is not given then $h_c = \frac{10.5}{2cy}$ whe push to had is interpreted by the second by th a) Find the low of head when the pipe of diamiter 200 mm is indolenlig enlarique, to a diameters of yoomm. The rate of flow of waler through the pipe in 250 litro/see. Le $D_1 = 200 \text{ mm} = 0.2 \text{ m}$ $130 D_2 = 400 \text{ mm} = 0.4 \text{ m}$. $A_{1} = \pi \sqrt{2} p_{1}^{2} = \pi \sqrt{2} (0.2)^{2} = 0.03141 m^{2}$ $A_{2} = \pi_{4} D_{2}^{2} = \pi_{4} \times (0.4)^{2} = 0.12564 m^{2}$ $cl = 250 lit n / s = 0.25 m^3 / s$. VI = 0/AI = 7.96 mg/s sub prod to Nobe di $v_2 = 0/A_2 = 1.99 m/J$, noisil- 10 prioda $h_{e} = \frac{(v_{1} - v_{2})^{2}}{2q^{2}} = \frac{(7 \cdot q_{6} - 1 \cdot q_{q})^{2}}{2\chi q \cdot 81} + \frac{(v_{1} - v_{2})^{2}}{2\chi q \cdot 81}$ = 1.816 m of 1 water. (Ans) = 1.816 m of 1 water. (Ans) 1 Evx websit of - REF sectioned and piper ray (63)

3) LOSA of Head at the Entrance of pipe. This is the low of every which occury when a liquid enters a pipe cohich is connected to large tank. $h_i = 0.5 \frac{\sqrt{2}}{29} = 0 = (1 - 1)^2$ v = relouity of liquid in pipe. 4) LOM of Head at the Gnit of pipe ... This is loss of head due to relocity of liquid at the outlet of pipe : 9th in denoted as ho $h_0 = \frac{v^2}{2g}$ v = velocity of liquid atoutlet of pipe.5> Loss of head due to Bend in pipe !when there is bend in pipe the nelocity of flow changes due to which formation of eddies $\int h_{b} = \frac{Kv^{2}}{2g} \int e^{-S(t' \cdot 0)K} \int h = Sec prime$ Source of a linear intervaltakes place. hb = low of head due to bend -~ = velocity of flow. K= wefficient of bend. 6} LOIN OF Head in Various pipe fittings This is the loss of head in various pipe fittings. 91 is expressed as KV2 2g V= mlouity -0 + flow. KE coefficient Of pipe Lill.

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HYDRAULIC GIRADIENT LINE -

9+ is defined as the line which gives the sum of pressure head (P/w) and datum head(2) of a flowing fluig in a pipe with respect to some references line. >9+ is briefly written as H.G.L (Hydraulic gradient Line) TOTAL ENERGY LINE!_

9+ in defined as the line which gives the run of pressure head, daturn head and renetic head of a flowing fluid in a pipe with respect to rome reference line. ->9+ is briefly written as FE.L (Total Energy Line).

IMPACT OF JET (CHAPTER-7) Impart of jet on a fined vertical flat plate F Start A pipe. Nozzle. K-Plate UK -romider a jet of water coming out from the nozzle, strikes a flat vertical plate. do () o philador y f V = relacity off, the jet - notes - man 10 porod = diameter of the jet and set in the period > The jet after striking the plate, will move along the plate. But the plate is at right angles to the jet. Hence the jet affer striking will get deflecter through 90°. rAfter striking the component of the velocity of jet in the direction of jet is zero. The force exercled by the jet on the plate in the direction of jet Fr = Rate of change of momentum in direction of force = Initial momentum-final momentum - (Mass X initial velocity) - (Mass X Final velocity) Marin production Time ; where it word = 11 = Mar (initial velocity - Final velocity) = moin (V.-0) 66

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> The work will be done by the jet on the place, Stist ju Haston au plate às moving. workdone = Force & velocity = Fx×U $w = fa(v-v)^2 \chi v$ enerted by a jet of coaler, on a series of varies Force Lynell-ERDUD /.) plates. jet of water. 790 actual practice, a large number of plates are mounted on the circumfercoinen of a wheel at a finer dirtanu -> The jet strikes a plate and due to the force energies by the jet on the plate, the wheel stands moving. N= nelocity of jet. d = diametere of jet. a = cron-netional arrea of. jet := Mjd² U = velocity of varie. (- v. v. v. -> Man of water perc second striking the services of -> jet strikes the place with a relacity = (V-V) T WY TO V

The force eventsed by the jet in the direction
of motion of place

$$F_{n} = moun \ \text{eff} \times (\text{initial velocity} - fin al velocity) = \frac{3 \text{ av} [(v - v) - 0]}{[F_{n} = \frac{3 \text{ av} (v - v)}{2}]}$$
workdore = Force x Different velocity

$$= \frac{3 \text{ av} (v - v) \times v}{[W = \frac{3 \text{ av} (v - v) \times v]}{[W = \frac{3 \text{ av} (v - v) \times v]}}$$
Hindic energy of the jet per second = $\frac{1}{2} \text{ mv}^{2}$

$$= \frac{1}{2} \frac{5 \text{ av} \times v^{2}}{[K = \frac{1}{2} \frac{\sqrt{3} \text{ av}^{3}}{\sqrt{2}}]}$$

$$Q = \frac{\text{workdone per second}}{[K \in \text{ peri}] \text{ second}]}$$

$$= \frac{3 \text{ av} (v - v) \times v}{\sqrt{2} \frac{\sqrt{2}}{\sqrt{2}}}$$

$$\frac{1}{\sqrt{2} \frac{3 \text{ av}^{3}}{\sqrt{2}}} = \frac{2 v (v - v)}{\sqrt{2}}$$

$$\frac{1}{\sqrt{2}} \frac{2 v (v - v)}{\sqrt{2}}$$

$$= 0$$

$$= \frac{3 \text{ av} (v - v)}{\sqrt{2}} = 0$$

$$= \frac{3 \text{ av} (v - 2v^{2})}{\sqrt{2}} = 0$$

$$= \frac{2 v - 3x 2v}{\sqrt{2}} = 0$$

$$= 2 v - 4v = 0$$

$$= 2 v = \frac{1}{2} v = \frac{1}{\sqrt{2}}$$

Manimum efficiency

$$\begin{aligned}
\eta_{max} &= \frac{2v(v-v)}{v^2} \\
&= \frac{2v(2v-v)}{(2v)^2} \\
&= \frac{2vxv}{yv^2} = \frac{1}{2} = \frac{50^{\prime}}{1}, \quad \underline{\qquad} \\
\end{bmatrix}$$

Impact on a moving curved plate -T (1) / 200 400 200 202+ a allow the autor alpho and philos in public in the angle CAAD March Budy of vary in the direction VITI - Vit Vri 0. Dere sei = farval 510-1.00 to point of VIII I TREEF WE WELDERING CUL > As the # jet strickes tangentially, the loss of energy due to impact of the jet will be zero. as the plate is moving, the velocity with which jet of water staines is equal to the relative velocity of the jet with respect to the plate. VI = velocity of the jet at inlet U1 = nelocity of vane at inlet Vry = relative velocity of jet and plate at 0 = vare angle (inlet). V2 = relouity of jet at outlet. U2 = velocity 0 + vare at outlet. Vriz = relative velocity 0.4 jet at outleet. 13 = black angle at outlet. $\phi = vane$ angle at outlet.

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Vw1 = velocity of whire let inlet Vwz = velocity of or whire let outlet VI, = velocity of I low at inlet Vf2 = velocity of flow at outlet. ABD and EGIH are called as velocity triangly at inlet and outlet. velouity triangle cet inlet :-Analysis of nelocity trainingle :-U1 = U2 = U = velocity of vare in the direction of notion. $\nabla \pi_1 \equiv \nabla \pi_2$ -> man of water striking vare per see = fav, a=area of jet of water. NR, = relative velocity at indet. > porce enerched by the jet in the direction of moti $F_{\pi} = \int \alpha \sqrt{r_1} \left(\sqrt{w_1 + \sqrt{w_2}} \right) \int dt \int dt \int dt$ $4 \neq 13 = 90^{\circ}$, $Vw_2 \neq 0 \neq 1000^{\circ}$ is complete $F_{x} = \int_{a}^{a} V_{\alpha_{1}} \times V_{\omega_{1}} dt = \int_{a}^{a} V_{\omega_{1}} dt = \int_{a}^{a} V_{\omega_{1}} dt = \int_{a}^{a} V_{\omega_{1}} dt =$ > Brois pobling angle man 20 prisaler = 10 $F_n = f \alpha V_{re_1} \left[V_{\omega_1} - V_{\omega_2} \right]$ Thus in genericity Fre can be written as $F_n = f_n V_{rr_1} \left[V_{w_1, \pm} V_{w_2} \right] \left[\int_{v_1 v_1} v_{w_2} \right] \left[\int_{v_1 v_2} v_{w_2} \right$ si - fanden under el right the suit fee ansa.

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+ workdone per sewnd on the vane by jet
=
$$F_{K} \times U$$

efficiency of jet: -
 $Q = \frac{\delta u \xi p u t}{Inp u t}$
 $= \frac{\delta u k p u t}{Un p u t}$
 $= \frac{\delta u v k (Vw_1 \pm Vw_2) \times U}{\frac{1}{2} m v_1^2}$
 $= \frac{\delta^2 u V k (Vw_1 \pm Vw_2) \times U}{\frac{1}{2} x \sqrt{a}}$
 $= \frac{\delta^2 u V k (Vw_1 \pm Vw_2) \times U}{\frac{1}{2} x \sqrt{a}}$
 $= \frac{(Vw_1 \pm Vw_2) \times U}{\frac{1}{2} x \sqrt{a}}$
 $\int I = \frac{2 u (Vw_1 \pm Vw_2)}{v_1^2}$

84.44

add a start